

5 **WIPER-TYPE PHASE SHIFTER WITH CANTILEVER SHOE AND**
 DUAL-POLARIZATION ANTENNA WITH COMMONLY DRIVEN PHASE SHIFTERS

REFERENCE TO RELATED APPLICATIONS

 This application incorporates by reference the disclosures of commonly owned
10 United States Patent Application Serial Number 10/290,838 entitled "Variable Power
 Divider" filed on November 8, 2002; United States Patent Application Serial Number
 10/226,641 entitled "Microstrip Phase Shifter" filed on August 23, 2002; United States
 Patent Application Serial Number 10/623,379 entitled "Vertical Electrical Downtilt
 Antenna" filed on July 18, 2003; and United States Patent Application Serial Number
15 10/623,382 entitled "Double-Sided, Edge-Mounted Stripline Signal Processing
 Modules And Modular Network" filed on July 18, 2003.

TECHNICAL FIELD

 The present invention relates to wireless base station antennas systems and,
20 more particularly, relates to a wiper-type phase shifter with a cantilever shoe and a
 dual-polarization antenna including commonly driven phase shifters.

BACKGROUND OF THE INVENTION

 The present invention represents an improvement over the phase shifters
25 described in commonly owned United States Patent Application Serial Number
 10/290,838 entitled "Variable Power Divider" filed on November 8, 2002 and United
 States Patent Application Serial Number 10/226,641 entitled "Microstrip Phase
 Shifter" filed on August 23, 2002, which are incorporated herein by reference. The
 relevant background technology described in those applications will not be repeated
30 here. In addition, the phase shifter described in this specification may be deployed in
 the dual-polarization antenna described in commonly owned United States Patent
 Application Serial Number 10/623,379 entitled "Vertical Electrical Downtilt Antenna"
 filed on July 18, 2003, which is also incorporated herein by reference. Again, the
 background technology relevant to this embodiment of the invention is described in
35 that application and will not be repeated here.

Generally, the market for wireless base station antennas is highly price and performance competitive. Therefore, there is an on-going need for cost effective techniques for providing the technical features desired for these antennas. For example, advancements that reduce the size, cost, complexity, or number of moving parts are generally desirable. Of course, accurate and repeatable performance, as well ruggedness, longevity and low maintenance costs are also desirable. Meeting these competing design objectives is particularly challenging with respect to the moving parts of the antenna, such as the phase shifters used for beam steering and in variable power dividers, which may also be used for beam steering.

In particular, conventional phase shifters have used a wiper arm that slides along a transmission media trace located on a backplane to implement a differential phase shifter. See, for example, Japanese publication number 06-326501, published 25 November 1994, naming Mita Masaki and Tako Noriyuki as inventors. This type of phase shifter can experience failure if the wiper arm loses electrical communication with the transmission media trace. Because wireless base station antennas are typically deployed outdoors on buildings or towers, they are subject to the variable stresses and dimensional changes induced by temperature changes, vibration and external forces of wind, and other types of environmental conditions and variations over extended periods of time. These conditions can cause relative dimensional changes to occur between the components of the phase shifter assembly that can result in changes in the degree of wiper contact with the transmission media trace. Changes in wiper contact, such as partial wiper arm separation, can result in operational performance changes of the antenna. In extreme cases, complete wiper arm separation can result in operational failure of the antenna.

One conventional approach to solving the wiper arm separation problem is shown in FIG. 1. This configuration includes a slot 1 through the backplane 2 adjacent to the transmission media trace 5 and a spring-loaded set screw 3 extending from the wiper arm 4 through the slot. This approach is very effective at maintaining electrical communication between the wiper arm 4 and the transmission media trace 5, but has the disadvantage of requiring a slot through the backplane 2. This is a problem because in a typically wireless base station antenna, the backplane serves as an exterior wall intended to keep out the weather elements. Cutting slots through the backplane can cause water to enter the antenna, which can cause the antenna to short, corrode, and freeze if the temperature drops. To solve this problem, the phase shifter shown in FIG. 1 does not use the backplane 2 as an exterior enclosure wall,

but instead houses the backplane in an enclosure 6 that includes a separate exterior wall 7. Providing this exterior wall in addition to backplane 2, as well as brackets for supporting the backplane within the enclosure 6, increases the cost and complexity of the antenna.

5 In addition, dual-polarization antennas typically include a duplication of actuator, transmission and radiating elements; one for each polarization. Outfitting dual-polarization antennas with beam steering phase shifters in the conventional manner likewise requires a duplication of the phase shifters and associated actuators. This type of duplication can be costly, particularly when the phase shifters are motor
10 driven, which is desirable for remotely controlled operation. It is often desired to vary the phase in a like manner for each polarization to achieve corresponding characteristics. For this reason, commonly operating the phase shifters in a coordinated manner advantageously eliminates duplicate components.

 Accordingly, there is an ongoing need for more cost effective systems for
15 implementing phase shifters for wireless base station antennas including dual-polarization antennas. There is a further need for phase shifters for dual-polarization antennas that eliminate the duplication of parts.

SUMMARY OF THE INVENTION

20 The present invention meets the needs described above in an antenna suitable for use as a wireless base station antenna that includes a wiper-type phase shifter with a cantilever shoe that ensures that the electrical contact on the wiper arm remains in electrical communication with the transmission trace located on the antenna backplane without relying to an element, such as a spring-loaded set screw,
25 that passes through the backplane. The cantilever shoe thus provides a wiper hold-down mechanism without requiring holes or slots through the backplane, which could allow rain or other elements to get inside the antenna enclosure. The cantilever shoe is also a small, light weight, low maintenance, and inexpensive wiper arm hold-down mechanism in comparison to larger, bulkier, more complex, and more expensive hold-
30 down mechanism employed previously. In addition, locating a motor for driving the wiper arm on the rear of the backplane opposite the location of the wiper arm advantageously avoids complicated linkage elements.

 The invention may also be embodied in a dual-polarization antenna that includes a wiper-type phase shifter for each polarization. The wiper arms define gear
35 portions that engage each other, which allow a single actuator, typically located on

the rear of the backplane opposite the location of the wiper arms, to drive both wiper arms in a coordinated manner. Each wiper arm of the dual-polarization antenna may also include a cantilever shoe to gain the benefit of this design, as described above.

Generally described, the invention may be realized in a phase shifter suitable
5 for use in an antenna, such as a wireless base station antenna, that includes a backplane carrying a transmission media trace, such as a two-conductor stripline media commonly known as a microstrip trace. The phase shifter also includes a wiper arm pivotally attached to the backplane and carrying a trace contact. An actuator pivots the wiper arm with respect to the backplane, and a signal conductor is
10 in electrical communication with the trace contact. The phase shifter also includes a cantilever shoe including a trace contact biasing element configured to bias the trace contact toward the transmission media trace to ensure that the trace contact located on the wiper arm remains in electrical communication with the transmission media trace located on the backplane. The trace contact biasing element typically includes
15 a spring-loaded plunger positioned adjacent to the trace contact.

In this manner, the cantilever shoe ensures that the trace contact remains in electrical communication with the transmission media trace without relying on an element that passes through the backplane, such as a spring-loaded set screw. The signal conductor of the phase shifter may also include a signal trace carried on the
20 backplane, and the wiper arm may include a signal contact electrically located between the signal conductor and the trace contact. For this configuration, the cantilever shoe also includes a signal contact biasing element configured to bias the signal contact toward the signal trace. For example, the signal contact biasing element may include a spring washer positioned adjacent to the signal contact.

25 Electrical communication between the transmission media on the backplane and the trace contact wiper arm can be direct, such that a direct current (DC) can flow between the elements. Alternatively, this connection may be capacitively coupled, such that only a varying signal can flow between the elements. In particular, a capacitive insulating layer, such as a low-loss dielectric sheet, can be located
30 between these electrical conductors to prevent the flow of DC signals. This type of insulating layer advantageously suppresses intermodulation signal products that can occur when the conductors are in direct contact with each other. Without this type of insulating layer, a measurable non-linear current-voltage relationship can develop over time due to corrosion and other environmental conditions.

The phase shifter may be operated manually or mechanically (or both), and it may be controlled locally or remotely (or both). Therefore, the actuator may include a knob for manually pivoting the wiper arm. Alternatively or additionally, the actuator may include a motor for mechanically pivoting the wiper arm. The phase shifter may also include a controller for remotely controlling the motor. Typically, the wiper arm is located on a front side of the backplane and the motor is located on the rear side of the backplane, preferably opposite the location of the wiper arm to minimize the complexity of the linkage between the actuator and wiper arm. The front side may also include radiating elements of an antenna array. The wiper arm may also define a gear section for mechanically linking the wiper to another component, such as a drive gear or another wiper arm. In particular, an antenna may include two phase shifters that each include wiper arms that engage each other in this manner to cause coordinated pivotal movement of the wiper arms. For example, each phase shifter may drive a circuit associated with a polarization of a dual-polarization antenna array.

The invention may also be deployed as an antenna system that includes an array of antenna elements and a wiper-type phase shifter with a cantilever shoe, as described above. The antenna system may also include a beam forming network in electrical communication with the phase shifter and producing a plurality of beam driving signals, and a signal distribution network delivering each beam driving signal to one or more associated antenna elements. In this configuration, the beam driving signals drive the antenna elements to form a beam exhibiting a direction that varies in response to pivotal movement of the wiper arm. In a particular embodiment, the phase shifter drives a variable power divider electrically located between the phase shifter and the beam forming network to produce complimentary amplitude voltage drive signals over a range of voltage amplitude division.

In addition, each antenna element may be a dual-polarization antenna element, and the antenna system may include a similar phase shifter, beam forming network, and signal distribution network for each polarization. In this case, each wiper arm may define a gear section, which is typically cut directly into a dielectric substrate of a printed circuit (PC) board of the wiper arm. The gear sections of the wiper arms for each polarization typically engage each other to cause coordinated pivotal movement of the wiper arms. The antenna system may also include a motor for mechanically pivoting the wiper arms and a controller for remotely controlling the motor. For example, the wiper arms may be located on a front side of the backplane

and the motor may be located on the rear side of the backplane, typically opposite to the location of the wiper arms.

Therefore, it will be understood that the invention may also be deployed as a dual-polarization antenna including a phase shifter for each polarization, in which
5 each phase shifter includes a wiper arm in sliding electrical communication with an associated microstrip trace. In this configuration, the wiper arms define gear portions engaging each other and causing the wiper arms to move in a coordinated manner. As noted above, the wiper arms are typically located on a front side of a backplane carrying the microstrip trace, and a motor for mechanically pivoting the wiper arms is
10 typically located on the rear side of the backplane. In addition, the phase shifter for each polarization may include a cantilever shoe for each wiper arm biasing the wiper arm toward its associate microstrip trace.

In view of the foregoing, it will be appreciated that the present invention avoids the drawbacks of prior wiper-type phase shifters and dual-polarization antennas
15 including wiper-type phase shifters. The specific techniques and structures for implementing wiper-type phase shifters with cantilever shoes and dual-polarization antennas with mechanically linked wiper arms, and thereby accomplishing the advantages described above, will become apparent from the following detailed description of the embodiments and the appended drawings and claims.

20

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is an exploded perspective view of a conventional wiper-type phase shifter including a wiper arm hold-down mechanism relying on a spring-loaded set screw that passes through a slot in the phase shifter backplane.

25 FIG. 2 is a top view of a pair of wiper-type phase shifters with cantilever shoe hold-down mechanisms in a first position.

FIG. 3 is a top view of the phase shifters of FIG. 2 in a second position.

FIG. 4 is a top view of the phase shifters of FIG. 2 in a third position.

FIG. 5 is a schematic diagram of a wiper-type phase shifter in electrical
30 communication with a hybrid junction circuit to provide a variable power divider.

FIG. 6 is a conceptual illustration of the problem of wiper arm separation occurring in a wiper-type phase shifter prior to fully seating the elements.

FIG. 7 is a conceptual illustration of a fully seated cantilever shoe to solve the problem of wiper arm separation illustrated in FIG. 6.

FIG. 8 is an exploded perspective top view of a phase shifter wiper arm with a cantilever shoe.

FIG. 9 is an exploded perspective bottom view of the phase shifter wiper arm of FIG. 8.

5 FIG. 10 is a block diagram of a remotely controlled vertical electrical downtilt antenna deployed as a wireless base station antenna.

FIG. 11 is a diagram illustrating a vertical electrical downtilt antenna with an adjustable tilt bias.

FIG. 12 is a functional block diagram of a vertical electrical downtilt antenna.

10 FIG. 13 is an exploded perspective view of a dual-polarization vertical electrical downtilt antenna including a pair of commonly driven wiper-type phase shifters with cantilever shoe wiper arm hold-down mechanisms.

FIG. 14 is a front view of a main panel for a vertical electrical downtilt antenna.

15 FIG. 15 is a perspective view of the front of a beam steering circuit attached to a section of an antenna backplane.

FIG. 16 is a perspective view of the back of the beam steering circuit of FIG. 15.

FIG. 17 is a perspective view of the top of a manual actuator for operating a wiper-type phase shifter.

20 FIG. 18 is a perspective view of the bottom of the manual actuator of FIG. 17.

FIG. 19 is an exploded perspective view of the manual actuator of FIG. 17.

FIG. 20 is a perspective view of the top of a motorized actuator for operating a wiper-type phase shifter.

25 FIG. 21 is a perspective view of the bottom of the motorized actuator of FIG. 20.

FIG. 22 is an exploded perspective view of the motorized actuator of FIG. 20.

DETAILED DESCRIPTION OF THE EMBODIMENTS

30 The present invention may be embodied in a wiper-type phase shifter for an antenna, such as a wireless base station antenna, that includes a cantilever shoe wiper arm hold-down mechanism. In particular, this type of phase shifter may be used to drive a beam steering circuit that controls the direction of a beam formed by the antenna, as in a vertical electrical downtilt antenna. However, the phase shifter may also be used to control beam steering in azimuth or any other desired direction.

35 In addition, the phase shifter may also be used to drive systems other than beam

forming and beam steering circuits, such as power dividers, analog amplifiers, beam shaping circuits, and any other circuit employing an analog phase shifter.

The present invention may also be embodied in a dual-polarization antenna including commonly-driven wiper-type phase shifters. In particular, the wiper arms of the dual-polarization antenna are mechanically linked to each other through gear faces cut directly into the printed circuit (PC) board substrate of the wiper arm. This allows a common motor to actuate both wiper arms in a coordinated manner, which is desirable for beam steering such as vertical electrical downtilt, in which a coordinated phase shift is applied to different sets of antenna elements. It should be appreciated that this same technique may be used to coordinate other types of wiper arms, such as those controlling different antenna sub-arrays, different beam shaping circuits, and so forth. Similarly, it will be appreciated that the wiper-type phase shifter could also be deployed in a single polarization antenna, and may also be used to coordinate phase shifters or other actuators used for other purposes.

Cutting the gear faces directly into the PC board substrate eliminates the need for a separate component having gear faces, and the need to mechanically couple this separate geared component to the wiper arm. The dual functionality of a wiper arm with integrated geared faces simplifies the mechanical assembly necessary to commonly drive wiper-type phase shifters and reduces the number of discrete components in the dual phase shifter assembly. This advantageously reduces the size, complexity, and cost of the wiper-arm assembly.

The specific wiper-type phase shifter described below is constructed using microstrip RF circuits deployed on dielectric PC boards. Although microstrip RF circuitry is desirable to accomplish a number of design objectives, it should be understood that portions of the antenna circuitry could be implemented using other types of RF conductors, such as coaxial cable, waveguide, air microstrip, or tri-plate stripline. In fact, certain components of a particular commercial dual-polarization antenna (e.g., phase shifter, variable power divider, power distribution network, and antenna elements) are constructed using microstrip while other components (e.g., beam forming network) are constructed using tri-plate stripline. Similarly, coaxial, air microstrip, and other type of RF links may be deployed as desired.

It should also be understood that the specific biasing elements employed in the cantilever shoe wiper arm hold-down mechanism include a spring-loaded plunger and a wave-shaped spring washer. However, other types of suitable biasing elements may alternatively be employed, such as leaf springs, curved wiper arms, compressible

materials, and the like. At the same time, it should also be appreciated that the drag imposed by the biasing elements on the wiper arm and the coefficient of friction of the contacting surfaces dictates, in large measure, the power rating of a motorized actuator. Accordingly, low-friction surfaces and a biasing element providing sufficient and not excessive force is preferred. In addition, biasing elements that facilitate smooth, non-binding wiper arm movement are also preferred. For these reasons, the spring-loaded ball-bearing plunger and spring washer biasing elements are specified for the embodiments described below.

Turning now to the figures, in which like numerals refer to similar elements throughout the several figures, FIG. 1 is an exploded perspective view of a prior art wiper-type phase shifter including a wiper arm hold-down mechanism relying on a spring-loaded set screw that passes through a slot in the phase shifter backplane. As described previously, this particular phase shifter includes wiper arm hold-down mechanism that relies on a spring-loaded set screw **3** extending from the wiper arm **4** through a slot **1** in the backplane **2**. Cutting slots through the backplane makes the backplane unsuitable as an exterior enclosure wall. Therefore, the backplane is mounted within an enclosure **6** that includes a separate exterior wall **7**. Providing this exterior wall in addition to backplane **2**, as well as brackets for supporting the backplane within the enclosure **6**, increases the cost and complexity of the antenna.

FIG. 2 is a top view of a pair of wiper-type phase shifters **10A** and **10B** with cantilever shoe hold-down mechanisms **12A** and **12B**, respectively, in a first position "A". This phase shifter avoids the drawback associated with the phase shifter described above through the use of a cantilever shoe wiper hold-down mechanism that ensures that the electrical contact on the wiper arm remains in electrical communication with the transmission trace located on the antenna backplane without relying to an element, such as the spring-loaded set screw **3** shown in FIG. 1, that passes through an opening, such as the slot **1**, through the backplane.

The phase shifters **10A** and **10B** include wiper arms **12A** and **12B**, respectively, that each have an associated cantilever shoe **14A** and **14B**, respectively. The wiper arms are formed from small sections of dielectric PC board etched with tin-coated copper traces forming microstrip transmission media segments. The dielectric PC board material may be a PTFE Teflon® laminate, a laminate impregnated with glass fibers, having a relative dielectric constant equal to 2.2 ($\epsilon_r = 2.2$). This material can be used to construct PC boards that will exhibit an effective dielectric constant of 1.85 ($\epsilon_{\text{eff}} = 1.85$) for microstrip transmission media segments

exposed to the PC board on one side and exposed to air on the other side and having a characteristic impedance value of 50 Ohms.

Each wiper arm **12A** and **12B** includes a gear portion, **16A** and **16B**, respectively, that engage each other. The gear portion may be a spur gear section having an involute tooth design. The tooth geometry in **16A** and **16B** is symmetric about the local axis of each tooth, each tooth is typically identical in shape, and the gear portion is typically the same for each gear. For this reason, the wiper arms are typically interchangeable with each other, which is desirable from the parts inventory, antenna assembly, and antenna maintenance perspectives. The symmetric gear geometry is advantageous due to the need to drive the wipers bi-directionally. The involute gear geometry can be fabricated using standard PC board milling equipment commonly known as routers. The involute gear has the desirable property that center-to-center distance errors do not translate into angular errors.

This respective engagement of the gear portions **16A** and **16B** allows both wiper arms to be pivoted in a coordinated manner using a common manual or motorized actuator. Referring to FIGS. 2-5, the wiper arms **12A** and **12B** can be moved continuously through a range of motion from a first sweep extent "B" shown in FIG. 3, through the center point "A" shown in FIG. 2, and to a second sweep extent "C" shown in FIG. 4. FIG. 5 shows this same feature on a schematic diagram. Typically, the center point "A" corresponds to a nominal or zero differential phase shift position, position "B" corresponds to a maximum differential phase shift in one direction (e.g., lagging a reference phase value), and position "C" corresponds to a maximum differential phase in the opposite direction (e.g., leading the a reference phase value). For a beam steering application, the beam direction typically varies in response to changes in the phase shifter setting. In other words, the phase shifter steers the beam. In particular, each phase shifter **10A** and **10B** may steer a main beam of one polarization of a dual-polarization antenna. Even more particularly, these phase shifters may effect vertical electrical downtilt of the antenna beams corresponding to both polarizations of the dual-polarization antenna in a coordinated manner.

FIG. 6 is a conceptual illustration of the problem of wiper arm separation occurring in wiper-type phase shifter, which is illustrated for a singly wiper phase shifter designated as phase shifter **10** for descriptive convenience. The phase shifter **10** includes a wiper arm **12** positioned above a backplane **18**. Generally, the wiper arm **12** or the backplane **18** may be slightly non-planar at time of manufacture, or they

may become so over time due to internal or external forces, such as the weather elements. In FIG. 6, this non-planar configuration is illustrated for conceptual purposes by an exaggerated warp of the backplane. This type of non-planar configuration or effect can cause the transmission media trace **20** carried by the backplane **18** to lose electrical communication with the trace contact **22** carried by the wiper arm **12**. To counteract this problem, the cantilever shoe **14** includes a trace contact biasing element **24**, in this example a spring-loaded plunger consisting of a spring **26** and ball bearing **28** located inside a cylindrical sleeve **30** that includes a lip sized to retain the ball bearing while allowing it to move reciprocally within the sleeve against the force of the spring.

The backplane **18** also carries a signal conductor **32**, in this example a microstrip transmission media circuit. However, it should be understood that other types of signal conductors may carry the signal to the phase shifter, such as a coaxial cable, air microstrip, or any other suitable type of RF signal conductor. To conduct a signal from the signal conductor **32** to the trace contact **22**, the wiper arm **12** carries a signal contact **34** positioned above the signal conductor. To ensure that the signal contact **34** remains in electrical communication with the signal conductor **32**, the cantilever shoe **14** includes a signal contact biasing element **36**, in this example a wave-shaped spring washer. The signal contact **34** and trace contact **22** are typically formed from microstrip and connected to each other with a microstrip trace carried on the wiper arm **12** that can be a dielectric substrate of a PC board.

As shown in FIG. 7, tightening the cantilever shoe **14** toward the wiper arm **12** brings the biasing elements **24**, **36** into contact with the wiper arm, and thereby forces the trace contact **22** toward the transmission media trace **20**, and forces the signal contact **34** toward the signal conductor **32**. This, in turn, ensures that the transmission media trace **20** remains in electrical communication with the signal conductor **32** while allowing the wiper arm to move pivotally to change the phase setting of the phase shifter **10**. It should be noted that the trace contact **22** and the transmission media trace **20** do not contact each other directly, but instead are capacitively coupled through a thin dielectric spacer **23**, such as an adhesive backed dielectric tape with a dielectric constant of approximately 3.5 manufactured by Shercon, Inc. of Santa Fe Springs, California. The dielectric spacer **23** prevents metal-to-metal contact and thereby reduces the resistance to wiper arm movement. The dielectric tape also avoids wear of the microstrip traces, prevents binding, and prevents the introduction of signal noise into the RF circuit. Likewise, the signal

contact **34** and the signal conductor **32** do not contact each other directly, but instead are capacitively coupled through the thin dielectric spacer **23**.

Referring to FIG. 7, the constituents of the phase shifter **10** are conveniently shown in cross section. The top layer **40** of the wiper arm **12** is the dielectric PC board substrate formed from glass-impregnated TEFLON® laminate, the next layer **42** is the tin-coated copper microstrip trace, and the next layer **44** is the dielectric spacer material. The next layer **46** is the tin-coated copper microstrip transmission media trace carried on the backplane **18**. The next layer **48** is the PC board substrate of the backplane, which is bonded to an aluminum base plate **52** using a thin dielectric adhesive layer **50**, typically the VHB acrylic transfer adhesive by 3M Corporation, of St. Paul, Minnesota. The body **54** of the cantilever shoe **14A** is typically manufactured preferably from a dielectric material and generally a suitable temperature-stable plastic, such as NYLON®, ULTEM® (30% glass-filled polyetherimide) manufactured by General Electric Company, or any other suitable substrate. The trace contact biasing element **24** may be a pin-nosed or a spherical ball-nosed plunger, such as a stainless steel "ball push-fit plunger," part number SPFB48, manufactured by Vlier Products, a division of Barry Controls, a part of the Hutchinson Group Company.

FIG. 8 is an exploded perspective view of the top of the phase shifter wiper arm assembly **80**, and FIG. 9 is a corresponding view of the bottom of the assembly. The assembly includes a push-fit retaining ring **82** for holding the assembly on an actuator shaft. The push-fit retaining ring is located above the cantilever shoe **54**, which supports the trace contact biasing element **24**, in this example a ball-nose plunger, and a D-ring sleeve **84** that receives the actuator shaft. The signal contact biasing element **36**, in this example a wave-shaped spring washer, surrounds the actuator shaft and is sandwiched between the cantilever shoe **54** and the PC board **86** of the wiper arm, which carries a microstrip trace **88** that includes the signal contact **90** and the trace contact **92** connected by a microstrip trace **94**. A gear face **96** is cut directly into the PC board **86** of the wiper arm. The microstrip trace **88** is covered by a dielectric spacer layer **98**, such as the Shercon tape specified above.

Alternatively, the dielectric spacer layer can be a solder mask type coating found in conventional PC board processing systems, or it can be a thin polyester film known as CPL™ manufactured by Arlon Materials for Electronics a Division of Bairnco Corp. of Orlando FL. The CPL™ structure can also include the microstrip trace conductors **88** as features defined from a standard PC board etch process.

As shown in FIG. 10, the phase shifters described above may be employed to steer the beam of a remotely- or locally-controlled vertical electrical downtilt antenna **110**, which is suitable for use as a wireless base station antenna. This antenna is equipped to perform vertical electrical downtilt of a beam **112** emitted by the antenna.

5 More specifically, the antenna **110**, which is typically mounted to a pole **114**, tower, building or other suitable support structure, includes an upright panel that supports a number of antenna elements. These antenna elements emit the beam **112** in a boresight direction **115** (shown in FIG. 11), which is the natural propagation direction of the beam when the signals emitted by the antenna elements are in phase. In the
10 particular example shown in FIGS. 10 and 11, the antenna **110** is mounted with its main panel oriented vertically, which generally results in a horizontal boresight direction. This is a typical mounting configuration for a wireless base station antenna.

From the horizontal boresight direction **115**, some mechanism is typically provided to direct the beam **112** downward toward the horizon. It is also desirable to
15 have adjustable beam downtilt so that the beam can be pointed toward a desired geographical coverage area where the beam will be received with appropriate strength and to discriminate against the transmission of signals to areas generally beyond the geographical coverage area. The antenna **110** is reciprocal and the properties of the antenna in a reception mode of operation are the same as for a
20 transmission mode at each frequency in the operational band of frequencies. The antenna **110** is configured to implement adjustable beam downtilt within a range Θ , that extends between two boundary beam pointing directions, Θ_1 and Θ_2 . The tilt range Θ , is also typically biased downward from the boresight direction. For example, the upper tilt boundary is typically set toward or just below horizontal, and the tilt
25 range Θ , typically extends to about five degrees downward. For example, tilt ranges from one to five degrees from horizontal, and from two to seven degrees from horizontal are typical for antenna arrays having twelve or more radiating elements. However, the selection of the tilt bias and tilt range is a design choice that may be changed from application to application.

30 In addition, the tilt bias may be fixed or adjustable. FIG. 11 illustrates the adjustable tilt bias alternative by showing three tilt bias angles for the antenna **110**. For an antenna with an adjustable tilt bias, this parameter may be altered manually or mechanically, and it may be controlled locally or remotely.

Referring again to FIG. 10, the beam tilt bias and the tilt angle within the
35 adjustable tilt range may be controlled in several different ways. For example, one or

more control knobs may be located on the antenna **110** itself, typically on the rear of the main panel. However, climbing the pole **114** to adjust the beam tilt may be inconvenient. Therefore, a local controller **116** may be located at a suitable location, such as the base of the pole or with the base transceiver station **118** (BTS). In this case, a motor, such as a servo or stepper motor **136**, drives the tilt control in accordance with control signals from the local controller **116**. The motor is typically mounted to the rear of the main panel of the antenna **110**, but could be located in any other suitable location. In addition, a remote controller **120** may be used to remotely control the beam tilt. For example, the remote controller **120** is typically connected to the local controller **116** by way of a telephone line **122** or other suitable communication system. The local and remote controllers may be any suitable control device, as are well known in the art.

FIG. 12 is a functional block diagram of the antenna **110**, which includes a beam steering circuit that includes a variable power divider **130**, which includes one or more wiper-type phase shifters, and a multi-beam beam forming network **140**. The variable power divider **130** divides a voltage signal **132** into two complimentary amplitude voltage drive signals, which provide inputs to the multi-beam beam forming network **140** (BFN). The beam forming network **140**, in turn, produces beam driving signals **142** that are transmitted by a power distribution network **160** to a multi-element antenna array **150**. The power distribution network **160** divides each beam driving signals as appropriate for delivery to an associated sub-array of the multi-element antenna array **150**. The power distribution network **160** also includes tilt bias phase shifters **144** and phase blurring phase shifters **145**, which manipulate the phase characteristics of the beam steering signals in a coordinated manner through transmission media trace length adjustment to implement beam tilt and sidelobe reduction.

The variable power divider **130** receives and divides a voltage signal **132** into two voltage drive signals V_1 and V_2 . The voltage signal **132** typically contains encoded mobile communications data and is provided through a coaxial cable that attaches to a connector on the antenna **110**, as is well known in the art. FIG. 5 (introduced previously) is a schematic illustration of the variable power divider **130**, which is described in greater detail in commonly owned United States Patent Application Serial Number 10/290,838 entitled "Variable Power Divider" filed on November 8, 2002, which is incorporated herein by reference. The variable power divider **130** uses a single adjustable control element **12A**, typically a microstrip wiper

arm, to divide the input voltage signal **132** into the voltage drive signals V_1 and V_2 , which have complimentary amplitude and substantially constant phase delay over the range of voltage amplitude division.

More specifically, the amplitudes of sum of V_1 and V_2 sum to the amplitude input voltage signal **132**, and vary inversely with each other as the power is divided between them. In particular, the power division ranges from 100% to V_1 and zero to V_2 when the adjustable control element **12A** is in the position labeled "C" on FIG. 5 to zero to V_1 and 100% to V_2 when the adjustable control element **12A** is in the position labeled "B" on FIG. 5. In addition, the power division varies smoothly between these two extremes as the adjustable control element **12A** is moved between the positions "B" and "C" with position "A" representing the 50% division point.

In addition to having complimentary amplitude, the voltage drive signals V_1 and V_2 exhibit matched phase (i.e., they continuously have substantially the same phase) and substantially constant phase delay through the variable power divider **130**. In other words, the phase characteristics of the voltage drive signals V_1 and V_2 with respect to each other, and with respect to the input voltage signal **132**, remains substantially constant as the power division varies through the range of power division. An actuator **136**, such as a control knob or motor, is used to move the adjustable control element **12A**, which in turn causes adjustment of the beam tilt. This is illustrated in FIGS. 5 and 12, in which the beam tilt position labeled "A" in FIG. 12 corresponds to the position "A" of the adjustable control element **12A** shown in FIG. 5; the beam tilt position labeled "B" in FIG. 12 corresponds to the position "B" of the adjustable control element **12A** shown in FIG. 5; and the beam tilt position labeled "C" in FIG. 12 corresponds to the position "C" of the adjustable control element **12A** shown in FIG. 5.

Referring to FIG. 12, the voltage drive signals V_1 and V_2 provide input signals to the multi-beam beam forming network **140**, which is typically configured as an orthogonal two-by-four beam forming network or a four-by-four Butler matrix with two of the input ports shunted to ground through impedance matching resistors. Both configurations, along with a number of other signal processing modules, are described in detail in commonly owned United States Patent Application Serial Number 10/623,382 entitled "Double-Sided, Edge-Mounted Stripline Signal Processing Modules And Modular Network" filed on July 18, 2003, which is incorporated herein by reference. Although the beam forming network **140** need not

be configured as a double-sided, edge-mounted module, this configuration results in many advantages.

It should be appreciated that the number of outputs of the beam forming network **140** typically corresponds to the number of antenna sub-arrays, and may therefore be altered in accordance with the needs of a particular application. Although antennas with four and eight sub-arrays are common, other configurations, such as three, five and six sub-arrays are also typical. Of course, any desired number of sub-arrays and a wide variety of beam forming networks may be accommodated.

FIGS. 13-16 are computer-aided design (CAD) to-scale illustrations of a particular commercial embodiment of the vertical electrical downtilt antenna **180**, which includes twelve dual-polarization antenna elements **182**. This antenna is designed for an operational carrier frequency of 1.92 GHz (which is the center frequency of the authorized US Personal Communication Services, PCS, wireless band), and the antenna elements are spaced 0.7 free-space wavelength apart, which is approximately 4.6 inches. The electrically conducting backplane **184** for this antenna is rectangular with dimensions 56 inches long by 8 inch wide [approximately 142cm by 20cm]. A sixteen-element antenna is correspondingly longer, 72 inches long by 8 inches wide [approximately 183cm by 20cm] to accommodate four additional antenna elements with the same spacing. The radome **186** fits over and attaches to the backplane.

The antenna **180** includes two mounting brackets **188A-B**, two coaxial cable antenna interface connectors **190A-B**, and an actuator knob assembly **192** connect to the rear side of the backplane **184**. The coaxial cable connectors **190A-B** receive coaxial cables supplying two input voltage signals **132** (shown on FIG. 12), one for each polarization of the dual-polarization antenna. A conducting ground plane on the underside of a main panel **196** is attached with a non-conducting adhesive **194** to the front side of the backplane **184**. The conducting ground plane of the main panel printed circuit (PC) board **196** is capacitively coupled to the backplane **184** for RF signal flow across the junction. The main panel **196** is a dielectric PC board etched with tin-coated copper traces that form transmission media segments carrying the voltage signals from the coaxial cables connectors **190A-B** to the antenna elements **182**. More specifically, the transmission media segments form two virtually identical beam steering and power distribution circuits **198A-B**, one for each polarization. The dielectric material of the main panel **196** may be PTFE Teflon®, as described previously.

Referring to FIGS. 5, 12 and 13, two variable power dividers **1102A-B** (one for each polarization -- element **130** on FIG. 12) and two power distribution networks **1104A-B** (one for each polarization -- element **160** on FIG. 13) are located on the main panel **196**, whereas two beam forming networks **1106A-B** (one for each polarization -- element **140** on FIG. 3) are implemented as double-sided, edge-mounted modules that are solder-connected to the main panel **196**. Two wiper arms **1108A-B** (one for each polarization -- element **12A** on FIG. 5) are pivotally attached to the variable power divider areas of the main panel **196**. The wiper arms **1108A-B** are formed on small dielectric PC boards with etched copper traces similar to the materials used to construct main panel (but without a ground plane), and are mechanically coupled to each other through dove-tail gears formed into rear portions of the wiper arms. This allows both wiper arms to be moved in a coordinated manner by the single actuator knob **192** (element **136** on FIG. 12). In motorized embodiments, the actuator knob assembly **192** is replaced by a small motor and mechanical drive, such as a servo or stepper motor, mounted to rear of the backplane **184**. The motor may be housed in a suitable enclosure and typically includes an associated electronics PC board assembly for electrical power and motor control.

In addition, for embodiments including variable tilt bias, a rack and pinion drive system with a separate motor is typically attached to the rear side of the backplane **184**. In specific embodiments, the tilt bias phase shifters may be implemented as gear-driven, trombone-type or wiper-type phase shifters, which are typically distributed in two rows (one for each polarization) along the main panel **196**. In addition, a single toothed rack moved by a single knob or motor driven gear can be used to turn all of the tilt bias phase shifters in a coordinated manner so that all of the antenna elements for both polarizations are tilt biased in a coordinated manner.

FIG. 14 is a front view of the main panel **196**. One of the antenna elements **182** is labeled for reference. The variable power dividers **1102A-B** and the power distribution networks **1104A-B** are shown a bit more clearly in this view. The wiper arms **1108A-B** are shown in the center of the main panel **196** but have not been labeled to avoid obscuring the figure. The beam forming modules **1106A-B** are difficult to see in this view because they are edge mounted to the main panel **196**.

FIG. 15 is a perspective view of the top side of the section of the antenna carrying the beam steering circuit, which includes the variable power dividers **1102A-B** and the beam forming modules **1106A-B**. This illustration provides a better view of the beam forming modules **1106A-B** and the wiper arms **1108A-B**. FIG. 16 is a

perspective view of the bottom side of this same section of the antenna, which shows the cable connectors **190A-B** and the control actuator **192**.

FIG. 17 is a perspective view of the top of a manual actuator **192**, and FIG. 18 is a perspective view of the bottom of the manual actuator showing the actuator shaft **194** which fits into the actuator arm sleeve **84** shown on FIGS. 8 and 9. A second non-actuated shaft **196** is also provided for mounting stability. FIG. 19 is an exploded perspective view of the manual actuator **192**, which includes a control knob **1900** connected to a drive shaft **1902** by two bolts **1904A-B**. The knob **1900** carries a ball-nose spring-loaded plunger **1906** that acts as a detent mechanism that removably fits into positioning holes on a face plate **1908**. The drive shaft **1902** fits through a flange bearing **1910** and into a housing **1912**. An optional non-driven shaft **1914** positioned parallel to the drive shaft **1902** extends from the underside of the face plate **1908** through a second flange bearing **1918** and into the housing **1912**. The non-driven shaft **1914** is held in place by an e-ring **1916** on the top side of the housing **1912**. E-rings **1920** and **1922** secure the drive shaft **1902** and the non-driven shaft **1914**, respectively, on the underside of the housing **1912**.

FIG. 20 is a perspective view of the top side of a motorized actuator **2000** for operating a wiper-type phase shifter, and FIG. 21 is a perspective view of the bottom side of the motorized actuator. FIG. 22 is an exploded perspective view of the motorized actuator, which is a motor-driven rotational actuator that mounts on the rear of the backplane in the same location as the manual actuator **192**, typically on the backplane opposite the beam forming circuit as shown in FIGS. 15-16. The motorized actuator **2000** includes a housing **2002** that supports cable connectors **2004A-B** and provides protection of the internal components from weather and debris. The housing **2002** is secured to a mounting plate **2006** through a gasket **2008** by a number of screws **2010** to form an enclosure. The mounting plate **2006**, in turn, is secured to the antenna backplane through a gasket **2012** by a number of screws **2014**. The enclosure houses a stepper motor **2016** supported by a pair of brackets **2018, 2020**.

In particular, the stepper motor may be a 1.8 degree stepper motor operating at 12 Volts, 0.4 Amperes, such as model no. SST42D manufactured by Shiano Kenshi Co. Ltd. The stepper motor **2016** is controlled by a custom designed and manufactured electronic control board (not shown) that is supported by the bracket **2018**. The motor drives a worm gear **2022** that is affixed to the output shaft of the motor by a sleeve **2024** and a set screw **2026**. The worm gear, in turn, drives a spur

gear **2028** that drives an actuator shaft that fits into the actuator arm sleeve **84** of the wiper arm, as shown on FIGS. 8 and 9. A potentiometer **2030** tracks the position of the stepper motor.

In view of the foregoing, it will be appreciated that present invention provides
5 significant improvements for implementing wiper-type phase shifters for wireless base station antennas including dual-polarization antennas. It should be understood that the foregoing relates only to the exemplary embodiments of the present invention, and that numerous changes may be made therein without departing from the spirit and scope of the invention as defined by the following claims.